

Investigation on the influence of the incidence angle on the reflectorless distance measurement of a terrestrial laser scanner



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Abstract

Although the influence of incidence angle (IA) is one of the known error influences of terrestrial laser scanners (TLS), it is not taken into account in the evaluation of TLS-data. In this paper the fundamental question is discussed, how the IA influences the TLS-distances, if the uncertainty is of stochastic or of systematic nature or of a combination of both. For this purpose, a new methodology has been developed. Its special feature is that the directly measured TLS-distances are compared with reference distances. It can be applied for close range and for longer distances. The methodology was realised with a time of flight laser scanner. At close range of 3.5 to 5.2m other error effects up to 4.4 mm are more pronounced than the influence of IA. At the distance of about 30 m, a systematic effect of IA was found. The total variation of the distance difference with IA is of ca. 2.0 mm. The stochastic properties of the influence of IA could not be quantified. In future works the methodology will be improved with respect to the obtained knowledge in order to quantify the error influence completely.

Keywords: Incidence angle, reflectorless distance measurement, laser scanner, scanning total station, close range, cyclic distance deviation

Kurzfassung

Obwohl der Einfluss des Auftreffwinkels (AW) zu den bekannten Fehlereinflüssen von terrestrischen Laserscannern (TLS) gehört, wird er bei der Beurteilung von TLS-Daten äußerst selten berücksichtigt. In diesem Paper wird eine grundsätzliche Frage behandelt, ob er stochastischer oder systematischer Natur ist oder eine Kombination von beiden darstellt. Dazu wurde eine neue Methodik entwickelt. Ihre Besonderheit besteht darin, dass die direkt gemessenen TLS-Distanzen mit Referenzdistanzen verglichen werden. Sie ist optional für den Nahbereich und für längere Entfernungen umsetzbar und wird hier mit einem impulslaufzeitbasierten TLS realisiert. Im Nahbereich von 3,5 bis 5,2m wirken sich andere Fehlereinflüsse mit Beträgen bis 4,4mm stärker auf die Distanzmessung aus als der AW. In der Entfernung von 30m wurde ein systematischer Effekt des AW festgestellt. Die Distanzänderung in Abhängigkeit vom AW beträgt ca. 2,0mm. Die stochastischen Eigenschaften des Einflusses des AW konnten nicht quantifiziert werden. Eine zukünftige Verbesserung der Methodik ausgehend von den gewonnenen Erkenntnissen soll eine vollständige Beschreibung dieses Fehlereinflusses gewährleisten.

Schlüsselwörter: Auftreffwinkel, reflektorlose Distanzmessung, Laser Scanner, scannende Total Station, Nahbereich, zyklische Distanzabweichungen

1. Introduction

In general, the geometry of object surfaces is determined from terrestrial laser scanning (TLS) measurements under varying incidence angles (IA). In consequence, the circular laser spot is deformed to an ellipse so that less signal strength is reflected back in comparison to its perpendicular alignment. The IA of the laser can affect the reflectorless distance measurements (RL) and thus, the TLS-data. In order to consider this influence in the TLS-measurement's planning as well as in the evaluation of TLS-data and in the

object modelling, the quantification of its impact is necessary.

Existing publications explain the influence of IA on the distance measurement (i) by the changing geometry in the laser-surface interaction, (ii) in view of the reflected signal strength from the measured surface and (iii) as a combination of both.

(i) The geometrically-based explanation is twofold: Due to the deformation of the laser spot the center of the ellipse does not match the geometric end-point of the distance, which may lead

to deviation of the measured distance [1, 2] or the average of the distances within the laser spot is longer compared to the distance measured in the spatial direction determined by the horizontal direction and the zenith distance [3].

(ii) Due to the dominant signal strength which is concentrated in the nearer part of the elliptical laser spot more signal is reflected back from this area of the laser spot. As a result, the near area is more heavily weighted in the mixed signal and leads to shorter distances [4, 5]. Alternative theory states that the geometrical change of the laser spot reduces the reflected signal strength [6, 7, 8] which in turn influences the distance measurement.

Previous investigations on the influence of IA on the distance measurement of TLS are characterised by three problems. First, the character of the error influence is not clear. In some studies it has been described by a correction term [1, 6, 9] which indicates a systematic nature and in others by a standard deviation which can indicate a stochastic [8] or a systematic character [3, 10]. Secondly, the impact was assessed by indirectly derived parameters. Aspects such as form and geometric quality of the measured objects, heterogeneous errors influencing the collected TLS-data and applied estimation algorithms can also falsify the quantified influence of the error. For the third the impact of the IA was quantified mainly at close range.

In this paper, the influence of IA on the RL measurement is quantified in such a way that the mentioned problematic aspects are minimised. The aim is to answer the fundamental question, whether the influence of the IA on the measured distances is of stochastic or of systematic nature or a combination of both.

A new methodology to investigate the error influence is introduced. Instead of deriving the parameters indirectly, the study is performed on the level of directly TLS-measured distances which are compared with reference distances. To investigate the error influence at greater distances, two variants of the method have been developed for close range and for longer distances. The method is suitable for scanning total stations (TLS+TS).

The proposed methodology is executed with a time of flight TLS. The realised measurement setups and measurement procedures are described in detail. After evaluation of the measured data, the results are analysed, evaluated and discussed in the framework of these research issue.

2. Methodology

Our investigations of the influence of IA are based on the direct comparison of the reference with the TLS-distance. The investigated TLS-distance D_{TLS} is defined as the distance between the zero point of TLS+TS and the scanned point P_i (see Figure 1).

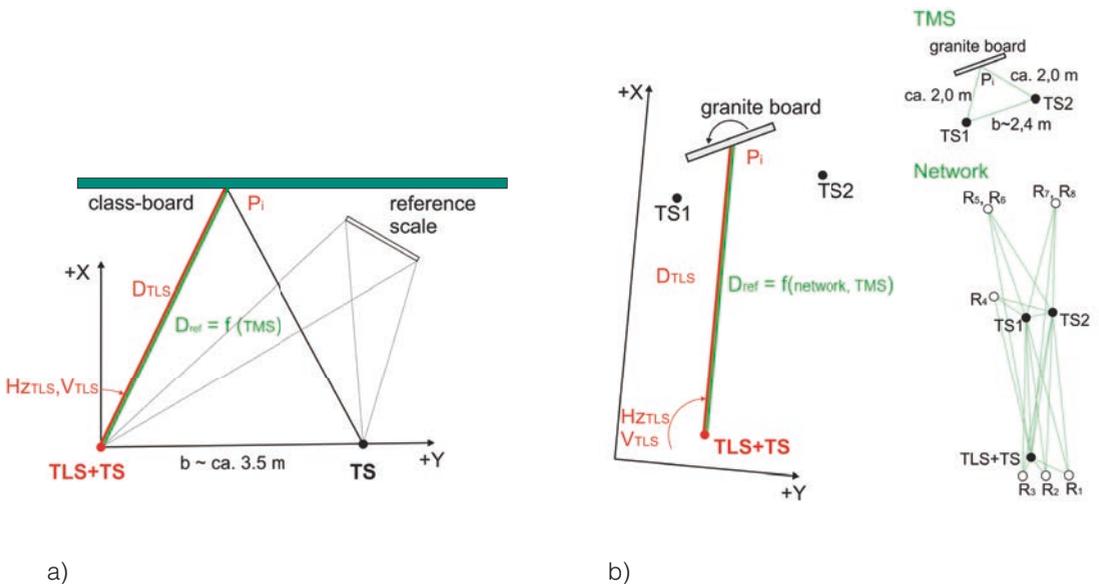


Fig. 1: Measurement setup a) for close range, b) for longer distance

The methodology consists of the following steps (Figure 1):

- 1) A planar object (class-board, granite board) is scanned from a standpoint of TLS+TS. The coordinates Y_{TLS} , X_{TLS} , Z_{TLS} of the point cloud are converted into polar coordinates $H_{\text{Z}_{\text{TLS}}}$, V_{TLS} , D_{TLS} (horizontal direction, zenith distance, distance).
- 2) The point on the object P_i is staked out via $H_{\text{Z}_{\text{TLS}}}$, V_{TLS} using the tacheometric part of the instrument TLS+TS and signalled. The fundamental condition must be fulfilled, that TLS and TS work in the same coordinate system.
- 3) The end points of the studied distance P_i are determined with a theodolite measurement system (TMS). Subsequently, the reference distance D_{ref} is calculated from the determined coordinates. The TMS consists of TLS+TS and another TS instrument (Figure 1 a).
- 4) For the investigation of the error influence at longer distances e. g. 30m it is not possible to use only the TMS due to the decrease of the accuracy and the spatial limitations in the laboratory. In this case, the object point P_i is determined with the TMS from a base b (TS1-TS2) which is located at a short distance to the planar object (approx. 1.6 m) (Figure 1b). The base points and the reference point of the scanner are determined in a geodetic high-precision network (TS1, TS2, TLS+TS, reflectors R_1 - R_8).
- 5) The variant for determining the reference distance is selected according to the a priori accuracy analysis. The reference should be at least one order of magnitude more accurate than the investigated distance.
- 6) Steps 2 and 3 are repeated for distances under different IA.
- 7) The character of the influence of IA will be investigated on the basis of the differences between the reference D_{ref} and TLS-distances D_{TLS} .

3. Measurements

The study was carried out with a Leica MultiStation MS50. It is characterised by the accuracy of the RL-distance measurement of 2mm + 2ppm, a distance measurement noise of 0.4mm up to 10m, 0.5mm up to 25m at measurement frequency of 62Hz and the angular accuracy of 0.3mgon. The spot size is 7×10 mm at 30m.

The MS50 was used at close range (3.5 to 5.2m) as well as at a distance of ca. 30m under laboratory conditions. The near field was chosen because instruments have special behaviour in this range. The distance of 30m belongs to usually measured distances at scanning of structures. Scanning was performed with the measuring rate of 62Hz. The scanning parameters were set in a way that avoids correlations between adjacent distances.

The measurement process is automated predominantly via GeoCOM control. In the following sub-sections the measurement setup and the measurement procedure of the two cases of investigations are described.

3.1 Experiment at close range

A wooden class-board was used as a test object (Figure 1 a). It has dark green color, dimensions of 5 m \times 1.5 m \times 0.025 m (width \times height \times depth) and is almost vertically fixed to the wall. The two station-points of the TMS were placed at 3.5m from the object. In this measurement setup the MS50 was simultaneously used as a theodolite within the TMS configuration. The base b between the theodolites (TLS+TS, TS) was 3.5m long. For the basis determination a reference scale of 0.8m was positioned horizontally.

Different IAs of the laser beam are obtained by the rotation of instrument's collimation axis in horizontal and vertical direction. In this measurement setup the TLS-distances vary from 3.5m at IA of 0gon to 5.2m at IA of 55gon.

In the measurement procedure first preparation steps were performed for TMS - mutual orientation of the horizontal circle of the theodolite and base determination. The mutual orientation was determined by collimation in two faces. Both instruments are specified with the same angular accuracy of $\sigma_{\text{Hz}} = 0.3$ mgon. The base was indirectly determined by solving the Hansen problem [11]. The length of the reference scale was measured with the laser interferometer Agilent 5530 with $\sigma_{\text{ref. scale}} = 0.4$ ppm. The pointing precision to targets of the reference scale with MS50 is 0.3mgon and with TS 0.3mgon at the first and 0.7mgon at the second end point (from 10 repetitions).

Subsequently, the board was scanned in one face with a resolution of 0.3700gon. The atmospheric corrections were applied to the distance measurement.

The obtained point cloud of the object was approximated by a plane. Hence, for each point the IA was calculated as the angle between the normal vector of the plane and the sighting line under $H_{z_{TLS}}$ and V_{TLS} . The IA calculated in this way varies from 0 to 55 gon. The point cloud was divided in 5-gon zones of IA and 7 points per zone were selected for further study of the distance.

Each selected point was staked out, the RL distance in the single mode D_{RL} was measured and the point was signalled with a needle. Its position was determined from Hz, V measurements performed in two faces from the two TMS-stations. The points located in two zones were determined twice, in order to empirically determine the precision of the staking out and of the reference measurement. A maximum deviation of two determinations of the reference distance of 0.4 mm was obtained by this procedure.

The stability of the stations was monitored during the measurement process; first by collimation, secondly by repeated measurements to surrounding prisms, and third by repeated base determination. Within a time interval of 2 months the measurements were performed with two different TLS+TS instruments using the same measuring setup and another measuring arrangement with a longer base of about 7 m as well.

3.2 Experiment at 30 m-long distance

The test object used in this case was a granite board with dimensions $0.40 \times 0.40 \times 0.03$ m (width x height x depth), that has a smooth and a rough side (Figure 2). It was placed nearly vertically on a Thorlabs board and fixed laterally. The Thorlabs board with weight of 30 kg and dimensions of $0.60 \times 0.60 \times 0.06$ m is sufficiently stable for the granite board.

The different IAs were obtained by rotating the object around its vertical axis. For this purpose, an angular scale was used. The TLS+TS was installed on a pillar about 30 m away from the test object. The distance between the two theodolites (TS1 and TS2) forming the TMS was 2.4 m. The base was placed at a distance of ca. 1.6 m from the object. The three instrument stations and the surrounding 8 prisms (R_i) mounted on consoles and pillars form the geodetic high-precision network.

The measurement campaign started with the determination of the precise network. During the



Fig. 2: Test object – granite board with four points for control measurement

entire campaign, the three instruments remained mounted in tribrachs to avoid centering errors. Therefore, with each instrument (TLS+TS, TS1, TS2) the elements Hz, V, D were measured to the prisms while only Hz, V were measured to the other instruments by the collimation in 3 sets. TS1 and TS2 have a specified angular accuracy of 0.3 mgon, TS1 the distance accuracy of $2 \text{ mm} + 2 \text{ ppm}$ and TS2 $1 \text{ mm} + 1.5 \text{ ppm}$.

For each IA the granite board was scanned with a resolution of 0.0212 gon in one face. Just as in close range it was then approximated by a plane. At each IA among all scanned points 5 per position were selected on the basis of their distance to the adjusted plane. Each selected point was staked out and signalled in the $H_{z_{TLS}}$, V_{TLS} direction. The 3D-position of the signalled point was determined in two faces with TMS. The granite board was aligned in steps of 10 (5) gon in order to get IA between 0 and 60 gon. The influence of the IA was studied on both sides of the granite board. At IAs of 0, 45, 55 gon staking out and TMS-measurements were realised twice, in order to quantify the precision.

By means of measuring 4 points on the board before and after staking out it was verified if the position of the board remained unchanged during the staking out and the reference measurement process (Figure 2). The stability of three stations was controlled by polar measurements to prisms and the Hz, V directions measurements between stations.

4. Post processing and results

The reference distances were determined from the highly accurate measurements. They meet the high accuracy requirement that is necessary in order to quantify the influence of the IA. Any systematic deviation affecting these measurements was first analysed. Based on this assessment the accuracy achieved for the reference range could be expressed. Furthermore, reference and TLS-distances were compared, the resulting distance differences were analysed and conclusions were drawn.

4.1 Investigation at close range

The reference distances are determined from the coordinates of the TLS + TS-zero point and of the selected object points. Errors that could possibly affect the obtained reference distance are listed in Table 1. They were methodically eliminated or quantified and their impact was evaluated. Based on this research we conclude that the reference distance could be systematically distorted up to ca. 0.2 mm.

The a priori standard deviation of the reference distance of 0.2 mm was obtained by simulation studies. This value conforms exactly to the empirical standard deviation of the reference distance, obtained from two independent repeated determinations of the reference distance in two zones.

The differences between the reference distances D_{ref} and the corresponding distances in the scanning mode D_{TLS} are shown in Figure 3a. The illustrated differences vary systematically with the IA. The scanned distances are up to 3.0 mm longer than D_{ref} in two intervals: 0–35 and 50–55 gon. In contrast, the distances are up to 4.4 mm shorter within the interval 35–50 gon. The shown systematic effect is physically or geometrically not-explainable. It was therefore assumed, that the obtained effect results from a superposition of the influence of IA with other effects in close range.

The systematic difference between the reference and the scanned distances was repro-

Influence	Impact/Elimination
Stability of the theodolite	1. Repeated measurement of 5 prisms max. coordinate difference of 0.5 mm – within the accuracy of the measurement method 2. Repeated collimation – emp. σ of 0.5 mgon 3. Repeated base determination σ of 0.1 mm, max. deviation of 0.3 mm Stable stations
Axes errors, eccentricity errors	Eliminated by measurements in two faces
Skewness of the trunnion axis	Min. impact at V directions from 95 to 105 gon
Collimation	Emp. σ of 0.5 mgon, max. deviation 1.2 mgon Max. impact on the reference distance 0.2 mm
Base determination	σ of 0.1 mm, max. deviation 0.3 mm
Hz, V – Scanning/Staking out	Max. deviation in Hz und V of 0.8 mgon Max. impact on the reference distance 0.02 mm No influence
Divergence of the line of sight and distance axis	Quantified in Tab. 2 at 30 m, at 5 m $\sim 1/6$ from max. deviation of 0.5 mm ~ 0.08 mm
Intersection angle	45–58 gon Measurement with another configuration with doubled base length No influence
Staking out/TMS	Repeatability of reference distance σ of 0.2 mm

Tab. 1: Error influences on the reference distance determination in close range

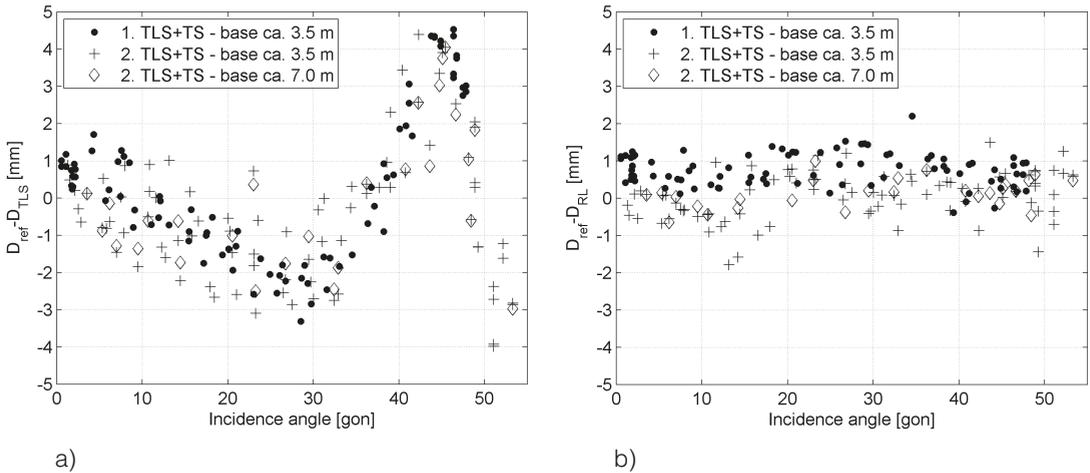


Fig. 3: Distance differences as function of the incidence angle; a) differences between D_{ref} and D_{TLS} (TLS-scanning mode), b) differences between D_{ref} and D_{RL} (RL-single mode)

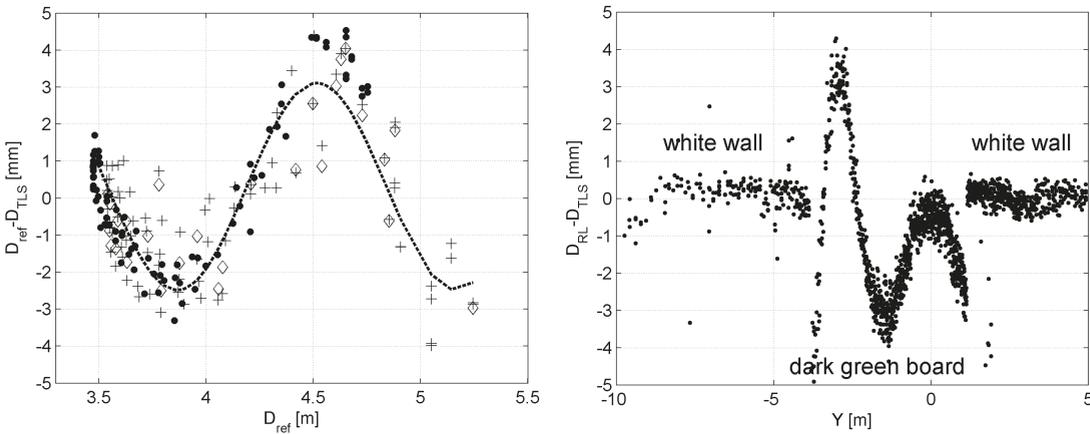


Fig. 4: Differences between D_{ref} and D_{TLS} as function of the distance

Fig. 5: Differences $D_{RL} - D_{TLS}$ as function of the material (abscissa Y-coordinate, almost parallel to the board)

duced 1.5 months later with another instrument of the same type using the same configuration as well as a slightly modified configuration with a longer base (Figure 3a).

If the systematic part of the distance deviation is split up using an appropriate approximating polynomial function, the stochastic properties in each zone of IA can be quantified. In this case, it is not relevant to express the precision as a function of the IA.

The differences between the reference distance and the reflectorless distance measurement in single mode $D_{ref} - D_{RL}$ show no systematic effects. The distance deviations are mainly in the interval of -1.0 mm to 1.5 mm , which cor-

responds to the manufacturer specification ($2\text{ mm} + 2\text{ ppm}$) (Figure 3b).

4.1.1 Systematic course in close range

To explain the occurred systematic effect in TLS-distance (Figure 3a) further analysis and experiments were performed. The conceptual connection of the investigations is:

- a) Determination of the distance dependence.
- b) Indication of the surface dependency.
- c) Determination of the colour dependence.

A) Distance dependence

In the experimental setup not only the IA varies, but also the distances. Therefore, the differences

$D_{\text{ref}} - D_{\text{TLS}}$ were plotted as a function of distance in Figure 4. Obvious distance dependence in the form of a cyclic oscillation can be noticed. However, this could not be a cyclic phase error because the instrument uses the time of flight method for distance measurements. To split up the influence of the distance a measuring arrangement with a fixed distance (minimal distance variation) and variable IA needs to be realised in the future.

B) Material dependence

The RL-distances measured in the single mode showed a good agreement with the TMS-distances (Figure 3b). For this reason in the following, the former are used as a reference basis for comparison. The board and parts of the adjacent white concrete wall have been scanned. The distances to some points were measured reflectorless in single mode (RL). The differences between RL- and scanned distances are shown in Figure 5 and indicate that the systematic effect is occurring only for the dark green board. Thus, the material dependence is evident. It should be noticed that the board has much lower reflectivity (8%) than the wall (90%) (empirically determined using Kodak gray card).

C) Dependency on the colour

Another board of the same colour and of another material consisting of a layer of glass and chip-board was examined as in the previous experiment B. In addition, different light colours were applied with chalk. The systematic differences

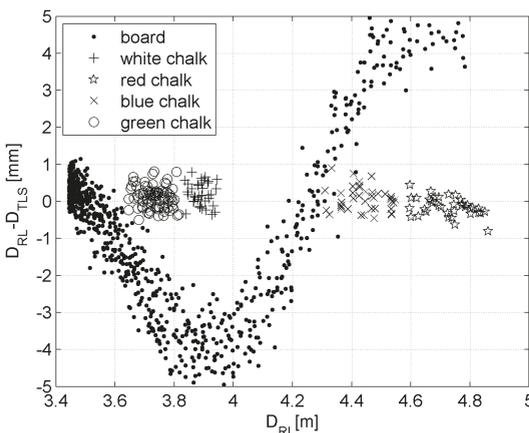


Fig. 6: Differences $D_{\text{RL}} - D_{\text{TLS}}$ as function of the distance, distances were measured to a surface of different colours

with the magnitude of ca. 4 mm occur only in case of dark green surfaces (Figure 6).

At the close range the systematic cyclic error effect influences TLS-distances. It occurs by scanning of dark green material.

A systematic material dependent effect at close range was also found in an earlier study [12] when measuring distances in single mode.

4.2 Investigation at a distance of 30 m

The reference distances D_{ref} were determined in two steps. First the coordinates of the intersection point of instrumental axes (zero point) were determined by a free adjustment of the high-precision network. Actual instrumental parameters were considered, which were determined by the method of ISO17123-4 [13]. The precision obtained for the position of zero points is (maximum values) $\sigma_Y = 0.03 \text{ mm}$, $\sigma_X = 0.14 \text{ mm}$, $\sigma_Z = 0.02 \text{ mm}$. These standard deviations seem to be optimistic due to the determination under repeatability conditions. However, they are representative for our case because the instruments remain fixed in the tribraches during the entire measurement campaign. Secondly the coordinates of object points P_i were calculated using spatial forward intersection with the base formed by TS1 and TS2.

The reference distances were obtained from the coordinates of the zero point of TLS+TS and of the determined object points.

Errors of the network measurement, the staking out and the TMS measurement affect the determined reference distance. Their contribution to the uncertainty of the reference distance is analysed and summarised in Table 2. The highest error influence is due to the staking out. In our case, if the granite board rotates around the vertical axis, stakeout precision in the horizontal direction directly affects the TLS-distance (e. g. a lateral deviation of 1.0 mm causes at an IA of 60 gon a distance error dD of 1.4 mm). This uncertainty is mainly caused by the thickness of the cross-hair and the magnification of the telescope. In future, the scale of the precise network e. g. the base should be controlled with high-accurate measurement.

The precision of the reference distance is calculated in the following way:

$$\sigma_{\text{ref}} = \sqrt{\sigma_{\text{NET_TMS}}^2 + \sigma_{\text{Stak}}^2}, \text{ where} \quad (1)$$

$$\sigma_{\text{Stak}} = \sqrt{\sigma_{\text{Stak_TMS}}^2 - \sigma_{\text{TMS}}^2}$$

	Influence		Impact/Elimination	
Precision network	Points definition	Stability of stations	1. Repeated measurement of 8 prisms - max. deviation in a coordinate of 0.7 mm 2. Hz, V - measurement between instrument stations – max. V - deviation of 1.3 mgon – max. Hz - deviation from the sum of the interior angles of the triangle (TLS+TS, TS1, TS2) 1.1 mgon – The individual Hz - directions vary within an interval of 2.5 mgon for TS1 and TS2, and of 0.9 mgon for TLS+TS; this results in a probable twisting of the Hz - circle (TS1 - 1.9 mgon, TS2 - 1.6 mgon) The internal geometry is preserved.	
			Centering error - instruments	Instruments remain in tribraches, Hz - and V - measurement through the collimation
			Centering error - prisms	Without removing
	Angle	Axes errors, eccentricity errors	Eliminated in two faces	
		Skewness of the trunnion axis	Object points are measured under vertical angles of 111 – 116 gon Network points are measured under vertical angles of 83 – 102 gon Close to the horizon, lower impact	
	Distance	Zero points errors	Considered	
		Scale error	Potential for improvement	
		Atmospheric corrections	Considered	
	Precision of station coordinates		max. $\sigma_Y = 0.03$ mm, $\sigma_X = 0.14$ mm, $\sigma_Z = 0.02$ mm	
	Staking out	Hz, V – Scanning/Staking out		max. dev. 0.6 mgon, lateral deviation of 0.3 mm, distance deviation of 0.4 mm under IA of 60 gon
Repeatability of staked out and with TMS determined distance		One point was staked-out 12 times under an IA of 55 gon, and determined with TMS $\sigma = 0.29$ mm		
Repeatability of staked out and with TMS determined distance		Twofold determination of the reference distances of 5 points under IA of 0, 40, 45, 55, 60 gon $\sigma = 0.05 - 0.51$ mm		
Divergence of the line of sight and distance axis		Distance measurement in single mode in two faces at IA = 60 gon, D = 30 m – rotation of the board clockwise and counterclockwise Max. distance deviation of 0.5 mm (incl. pointing uncertainty)		
TMS	Precision of azimuth R_{TS1_TS2}		$\sigma = 0.1$ mgon	
	Precision of base		$\sigma = 0.07$ mm	
	Angle errors		As in the network	
	Twisting of the Hz-circle at TS1 and TS2		Max. difference of the reference distance of 0.02 mm	
	Board stability – before/after staking out		4 points were measured with TMS before and after staking out Max. coordinate deviation of 0.05 mm	
	Repeatability of the distance determination by TMS		1 point signalled with the needle once and measured 12 times by TMS $\sigma = 0.01$ mm	

Tab. 2: Error influences on the reference distance determination at 30 m

σ_{Net_TMS} – standard deviation of the reference distance (TLS+TS, P_i) derived with variance propagation law by taking into account full covariance matrix of the network adjustment (0.17 mm),

σ_{Stak} – empirical standard deviation of the staked out reference distance,

σ_{Stak_TMS} – empirical standard deviation of the repeatedly staked out and with TMS determined reference distance (0.05 – 0.51 mm),

σ_{TMS} – empirical standard deviation of the once signalled and repeatedly with TMS determined reference distance (0.01 mm);

IA [gon]	0	40	45	55	60
Rough surface	0.18	0.45	—	0.27	—
Smooth surface	0.18	0.24	0.52	0.22	0.54

Tab.3: Standard deviation of the reference distance [mm]

The precision of the reference distance varies between 0.18 and 0.54 mm (Table 3).

The individual distance differences for both sides of the granite board are shown in Figure 7. In order to suppress the measurement noise, the distance differences per IA were averaged. The empirical standard deviations of a distance difference per IA reach values between 0.3 and 1.0mm. The standard deviations of the mean values are between 0.1 to 0.4mm. The averaged differences between the reference and TLS-distances at each IA are illustrated in Figure 8. Comparing the mean values with their

standard deviations we conclude according to the 3Sigma-rule (P = 99.7%) that the deviations are significant (Figure 8).

The differences (Figure 8) have a distance offset at IA 0 gon and vary systematically with the IA. At the rough surface of the granite board the TLS distance is 0.8 mm longer at AW 0 gon. This difference increases at larger IA up to 2.5 mm. The total variation of the distance difference with IA is of 1.7 mm. The smooth surface shows a similar behavior. At an IA of 0 gon the TLS distances are longer by 1.1 mm. At 60 gon the difference achieves 3.1 mm. Its total variation is of 2.0 mm.

The significant offset (at the rough surface - not significant at P = 99.7%) in the case of IA = 0 gon is surprising and needs further investigation. This IA is ideal for the RL measurement. The offset can be caused by other error influences on the RL distance measurement such as the reflectivity of the surface or the penetration of the laser [14].

The obtained systematic variation of the distance differences is caused most probably by the influence of the IA on the TLS distance measurement. Higher IA lead to worse geometrical and physical conditions, resulting in greater distance distortion. As in the case of the close range investigation the variation of the differences is strongly correlated with the received signal strength (Figure 9). Both, the distance differences and the received signal strengths are shifted (Figure 8 and 9). They also point to the influence of the surface roughness. The TLS-distances differences to the smooth surface are in average 0.7 mm longer than the ones for the rough surface.

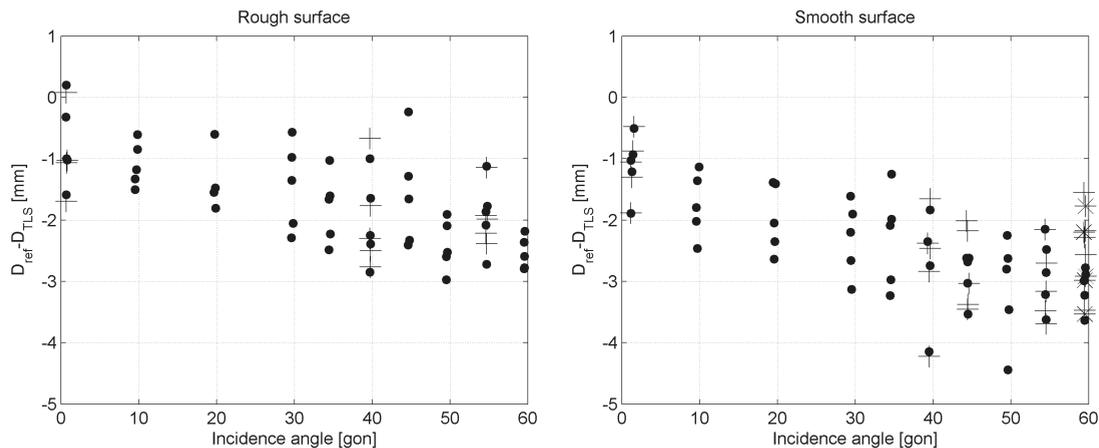


Fig. 7: Differences D_{ref} and D_{TLS} as function of the incidence angle (repeated determination – cross, star)

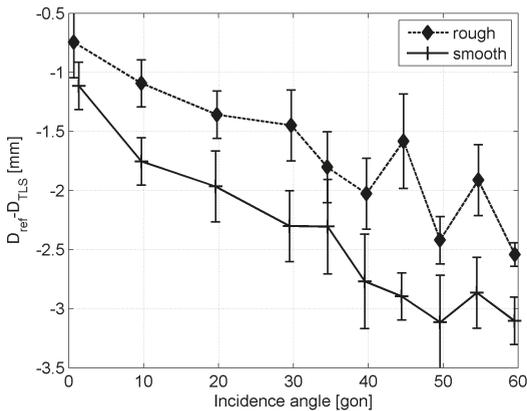


Fig. 8: Mean value of differences D_{ref} and D_{TLS} per one incidence angle and their standard deviations

In order to quantify the stochastic properties of the distances measured under various IA, we have assumed that the reference distances are more precise than D_{TLS} . Under this condition, the systematic component should be separated and the standard deviations calculated with respect to the IA. However, in our experiment this basic assumption was not met. Thus, the stochastic properties of the distances among IA is not quantified. This lack of the presented methodology needs to be eliminated in future works.

5. Conclusion and outlook

In this paper, a new method for investigating the influence of IA on the reflectorless distance measurement of scanning total stations was presented. It is new and unique by comparing the directly measured scanned distances to the reference in the areal acquisition. It is variable for distances of different lengths and was applied here for two ranges.

At close range of 3.5 to 5.2m it was found out that other errors are more pronounced than the IA. A systematic cyclic distance-dependent effect up to 4.4 mm was detected at a material of dark green color with low reflectivity. Its physical cause needs to be clarified in the future. It has been shown that in the realised measurement configuration with a fixed object, the variation of the investigated TLS-distances should be minimised or even eliminated. As a result, the object should not be fixed but rotatable.

At the distance of 30 m a systematic effect of IA was detected. In the range of IAs between 0 and 60 gon the distances differences between

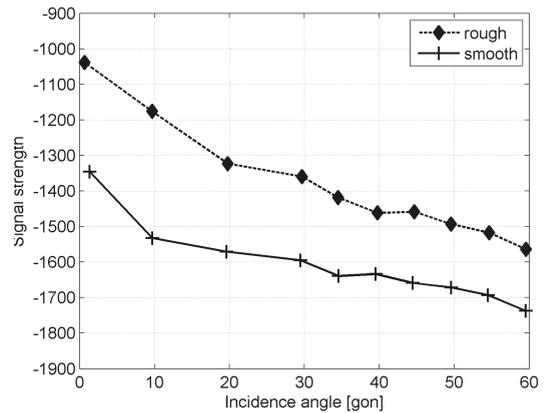


Fig. 9: Mean value of received signal strength by scanning to the rough and smooth surface of the granite board

reference and TLS vary up to 1.7 mm on the rough side and up to 2.0 mm on the smooth side of the granite board. The variation of the distance differences is closely related to the received signal strength. In addition, at IA of 0 gon a distance offset of -0.8 mm for the rough surface and -1.1 mm for the smooth surface could be detected. The stochastic properties of the error influence could not be quantified because the reference distances are too noisy. From the realised investigation it can be concluded that the uncertainty of the reference distance should be increased, especially the precision of the staking-out should be minimised. For the determination of the stochastics the methodology could be added to repeat scanning of the object in the identical Hz and V grid. From the repeated distance measurements stochastic properties of the error influence can be obtained.

The first experiences show that the developed methodology for investigating the influence of the IA has great potential. In future work the methodology will be improved with respect to the above mentioned shortcomings.

References

- [1] Lindstaedt, M., Kersten, T., Mechelke, K., Graeger, T., Sternberg, H. (2009): Phasen im Vergleich - Erste Untersuchungsergebnisse der Phasenvergleichsscanner FARO Photon und Trimble GX. In: Photogrammetrie, Laserscanning, Optische 3D-Messtechnik - Beiträge der Oldenburger 3D-Tage 2009, Wichmann Verlag, Heidelberg, pp. 53–64.
- [2] Schulz, T. (2007): Calibration of a Terrestrial Laser Scanner for Engineering Geodesy. Dissertation ETH, Zürich. In: http://www.geometh.ethz.ch/people/former_staff/schulzt/TS_PhD_Final.pdf

- [3] *Gordon, B. (2008a):* Zur Bestimmung von Messunsicherheiten terrestrischer Laserscanner. Dissertation, Technische Universität Darmstadt. In: http://tuprints.ulb.tu-darmstadt.de/1206/1/Dissertation_BGordon.pdf
- [4] *Joeckel, R., Stober, M., Huep, W. (2008):* Elektronische Entfernungs- und Richtungsmessung und ihre Integration in aktuelle Positionierungsverfahren. 5. Auflage, Wichmann Verlag, Heidelberg.
- [5] *Kern, F. (2003):* Automatisierte Modellierung von Bauwerksgeometrien aus 3D-Laserscanner-Daten. Dissertation, Geodätische Schriftenreihe der Technischen Universität Braunschweig (19).
- [6] *Kersten, T., Mechelke, K., Lindstaedt, M., Sternberg, H. (2008):* Geometric Accuracy Investigations of the Latest Terrestrial Laser Scanning Systems. In: CD-Proceedings, FIG Working Week, Stockholm, Sweden, June 14-19, 2008.
- [7] *Schäfer, T., Schulz, T. (2005):* Kalibrierung, Einflussgrößen und Genauigkeiten von Terrestrischen Laserscannern. In: Terrestrisches Laserscanning (TLS), Schriftenreihe des DVW (48), Wißner Verlag, Augsburg, pp. 29-48.
- [8] *Soudarissanane, S., Lindenberg, R., Menenti, M., Teunissen, P. (2011):* Scanning geometry: Influencing factor on the quality of terrestrial laser scanning. ISPRS Journal of Photogrammetry and Remote Sensing 66 (2011), pp. 389-399.
- [9] *Mechelke, K., Kersten, T., Lindstaedt, M. (2007):* Comparative Investigation into the Accuracy Behaviour of the New Generation of Terrestrial Laser Scanning Systems. In: Optical 3-D Measurement Techniques VIII., Zürich, pp. 319-327.
- [10] *Gordon, B. (2008b):* Diskussion von Feldprüfverfahren zur Messunsicherheitsbestimmung für terrestrische Laserscanner. In: Terrestrisches Laserscanning (TLS 2008), Schriftenreihe des DVW (54), Wißner Verlag, Augsburg, pp. 125-142.
- [11] *Witte, B., Sparla, P. (2011):* Vermessungskunde und Grundlagen der Statistik für das Bauwesen. Wichmann Verlag, Berlin, pp. 662-665.
- [12] *Juretzko, M. (2006):* Leistungsfähigkeit des reflektorlosen Distanzmessmoduls R300 der Tachymeterserie TPS1200 von Leica. Flächenmanagement und Bodenordnung (FuB), 2/2006, pp. 90-95.
- [13] *ISO17123-4 Optics and optical instruments - Field procedures for testing geodetic and surveying instruments - Part 4: Electro-optical distance meters (EDM measurements to reflectors).*
- [14] *Zámečnicková, M., Wieser, A., Woschitz, H., Ressler, C. (2014):* Influence of surface reflectivity on reflectorless electronic distance measurement and terrestrial laser scanning. Journal of Applied Geodesy, 8 (2014), 4, pp. 311-325.

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